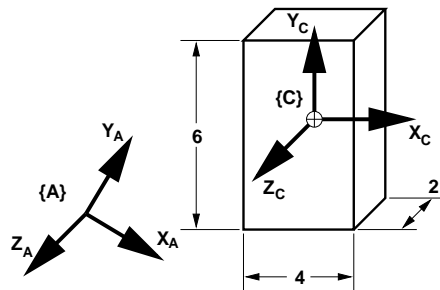


1. (a) Derive a formula that transforms an inertia tensor given in some frame  $\{C\}$  into a new frame  $\{A\}$ . The frame  $\{A\}$  can differ from frame  $\{C\}$  by both translation and rotation. You may assume that frame  $\{C\}$  is located at the center of mass.
- (b) Consider, for example, the uniform density box shown below. It has mass  $m = 12kg$ , and dimensions  $6 \times 4 \times 2$ :



Frame  $\{C\}$  lies at the center of mass of the box, and the coordinate axes are lined up with the principal axes of the box. In other words,  $\mathbf{Y}_C$  is aligned with the long axis of the box, and  $\mathbf{X}_C$  and  $\mathbf{Z}_C$  are aligned with the short axes of the box.

Compute the inertia tensor of the box in frame  $\{C\}$ .

*Note: For a frame located at the center of mass and oriented along the principal axes, the inertia tensor for the box of uniform density takes the form:*

$${}^C I = \begin{bmatrix} \frac{m}{12}(s_y^2 + s_z^2) & 0 & 0 \\ 0 & \frac{m}{12}(s_x^2 + s_z^2) & 0 \\ 0 & 0 & \frac{m}{12}(s_x^2 + s_y^2) \end{bmatrix}$$

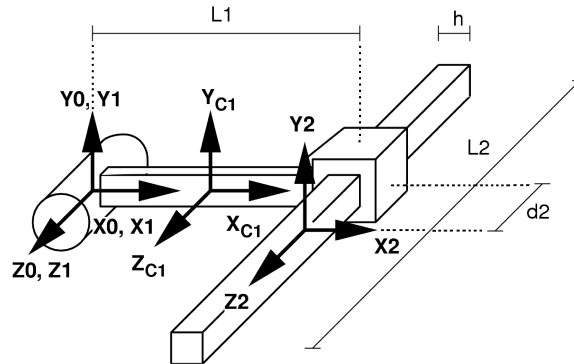
where  $s_x$ ,  $s_y$  and  $s_z$  are the dimensions of the box along the  $\mathbf{X}_C$ ,  $\mathbf{Y}_C$  and  $\mathbf{Z}_C$  axes, respectively.

- (c) Given the transformation matrix from  $\{C\}$  to  $\{A\}$ :

$${}^A T_C = \begin{bmatrix} \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 & 1 \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 0 & 1 \\ 0 & 0 & 1 & 2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

use your formula from part (a) and your inertia tensor from part (b) to compute the inertia tensor of the box in frame  $\{A\}$ .

2. In the rest of this problem set, we will walk through the process of finding the equations of motion for a simple manipulator from the Lagrange formulation. Consider the RP spatial manipulator shown below. The links of this manipulator are modeled as bars of uniform density, having square cross-sections of thickness  $h$ , lengths of  $L_1$  and  $L_2$ , and total masses of  $m_1$  and  $m_2$ , with centers of mass shown. Assume that the joints themselves are massless.



From the derivation in the Lecture Notes, we know that the equations of motion have the form:

$$M(\mathbf{q})\ddot{\mathbf{q}} + C(\mathbf{q})\dot{\mathbf{q}}^2 + B(\mathbf{q})[\dot{\mathbf{q}}\dot{\mathbf{q}}] + \mathbf{G}(\mathbf{q}) = \boldsymbol{\tau}$$

where  $M$  is the mass matrix,  $C$  is the matrix of coefficients for centrifugal forces,  $B$  is the matrix of coefficients for Coriolis forces, and  $\mathbf{G}$  is the vector of gravity forces.

- (a) For each link  $i$ , we have attached a frame  $\{C_i\}$  to the center of mass (in this case, frame  $\{2\}$  is the same as  $\{C_2\}$ ). Compute kinematics for these frames: that is, calculate the matrices  ${}^0C_1T$  and  ${}^0C_2T$ .

For a two-link manipulator, the mass matrix has the form

$$M = m_1 J_{v_1}^T J_{v_1} + m_2 J_{v_2}^T J_{v_2} + J_{\omega_1}^T C_1 I_1 J_{\omega_1} + J_{\omega_2}^T C_2 I_2 J_{\omega_2}$$

where  $J_{v_i}$  is the linear Jacobian of the center of mass of link  $i$ ,  $J_{\omega_i}$  is the angular velocity of link  $i$ , and  ${}^{C_i}I_i$  is the inertia tensor of link  $i$  expressed in frame  $\{C_i\}$ .

- (b) Calculate  ${}^0J_{v_1}$  and  ${}^0J_{v_2}$ .  
(c) Calculate  ${}^{C_1}J_{\omega_1}$  and  ${}^{C_2}J_{\omega_2}$ .  
(d) Calculate  ${}^{C_1}I_1$  and  ${}^{C_2}I_2$  in terms of the masses and dimensions of the links. You can use the same formula that was given for a box of uniform density in Problem 2(b). Be careful which measurements you use along the axes.  
(e) Calculate the mass matrix,  $M(\mathbf{q})$ . To make your algebra easier, leave the inertia tensors in symbolic form until the end, i.e.

$${}^{C_1}I_1 = \begin{bmatrix} I_{xx1} & 0 & 0 \\ 0 & I_{yy1} & 0 \\ 0 & 0 & I_{zz1} \end{bmatrix}$$

Now we need to calculate the centrifugal and Coriolis forces. We will derive the form directly.

(f) Beginning with the equation in the Lecture Notes,

$$\mathbf{v}(\mathbf{q}, \dot{\mathbf{q}}) = \dot{M}\dot{\mathbf{q}} - \frac{1}{2} \begin{bmatrix} \dot{\mathbf{q}}^T \frac{\partial M}{\partial q_1} \dot{\mathbf{q}} \\ \dot{\mathbf{q}}^T \frac{\partial M}{\partial q_2} \dot{\mathbf{q}} \end{bmatrix},$$

manipulate this equation symbolically into the form

$$\mathbf{v}(\mathbf{q}, \dot{\mathbf{q}}) = C(\mathbf{q})[\dot{\mathbf{q}}^2] + B(\mathbf{q})[\dot{\mathbf{q}}\dot{\mathbf{q}}]$$

where  $C$  and  $B$  are matrices in terms of the partial derivatives  $m_{ijk}$  of the mass matrix. Don't actually substitute in your answer from part (e) into this equation yet: just leave the elements of these matrices in  $m_{ijk}$  symbolic form.

(g) Using your answer to part (e), compute the matrices  $C(\mathbf{q})$  and  $B(\mathbf{q})$  in terms of the masses, dimensions, and configuration  $\mathbf{q}$  of the manipulator.

The last thing that remains is to derive the gravity vector  $\mathbf{G}(\mathbf{q})$ .

(h) Calculate,  ${}^0\mathbf{G}(\mathbf{q})$ , the gravity vector in frame  $\{0\}$ , in terms of the masses, the configuration  $\mathbf{q}$ , and the gravity constant  $g$  ( $g$  is positive). Assume that gravity pulls things along the  $-\mathbf{Z}_0$  direction. Be careful with your signs.

(i) As a final step, use your answers to parts (e), (h) and (i) to write out the equations of motion as two great big equations:

$$\begin{aligned} \tau_1 &= f_1(\ddot{\mathbf{q}}, \dot{\mathbf{q}}, \mathbf{q}) \\ \tau_2 &= f_2(\ddot{\mathbf{q}}, \dot{\mathbf{q}}, \mathbf{q}) \end{aligned}$$